NASA/TM-2003-212150



Membrane Vibration Tests Using Surface-Bonded Piezoelectric Patch Actuation

James L. Gaspar and Richard S. Pappa Langley Research Center, Hampton, Virginia

The NASA STI Program Office . . . in Profile

Since its founding, NASA has been dedicated to the advancement of aeronautics and space science. The NASA Scientific and Technical Information (STI) Program Office plays a key part in helping NASA maintain this important role.

The NASA STI Program Office is operated by Langley Research Center, the lead center for NASA's scientific and technical information. The NASA STI Program Office provides access to the NASA STI Database, the largest collection of aeronautical and space science STI in the world. The Program Office is also NASA's institutional mechanism for disseminating the results of its research and development activities. These results are published by NASA in the NASA STI Report Series, which includes the following report types:

- TECHNICAL PUBLICATION. Reports of completed research or a major significant phase of research that present the results of NASA programs and include extensive data or theoretical analysis. Includes compilations of significant scientific and technical data and information deemed to be of continuing reference value. NASA counterpart of peerreviewed formal professional papers, but having less stringent limitations on manuscript length and extent of graphic presentations.
- TECHNICAL MEMORANDUM. Scientific and technical findings that are preliminary or of specialized interest, e.g., quick release reports, working papers, and bibliographies that contain minimal annotation. Does not contain extensive analysis.
- CONTRACTOR REPORT. Scientific and technical findings by NASA-sponsored contractors and grantees.

- CONFERENCE PUBLICATION. Collected papers from scientific and technical conferences, symposia, seminars, or other meetings sponsored or co-sponsored by NASA.
- SPECIAL PUBLICATION. Scientific, technical, or historical information from NASA programs, projects, and missions, often concerned with subjects having substantial public interest.
- TECHNICAL TRANSLATION. Englishlanguage translations of foreign scientific and technical material pertinent to NASA's mission.

Specialized services that complement the STI Program Office's diverse offerings include creating custom thesauri, building customized databases, organizing and publishing research results ... even providing videos.

For more information about the NASA STI Program Office, see the following:

- Access the NASA STI Program Home Page at http://www.sti.nasa.gov
- E-mail your question via the Internet to help@sti.nasa.gov
- Fax your question to the NASA STI Help Desk at (301) 621-0134
- Phone the NASA STI Help Desk at (301) 621-0390
- Write to: NASA STI Help Desk NASA Center for AeroSpace Information 7121 Standard Drive Hanover, MD 21076-1320

NASA/TM-2003-212150



Membrane Vibration Tests Using Surface-Bonded Piezoelectric Patch Actuation

James L. Gaspar and Richard S. Pappa Langley Research Center, Hampton, Virginia

National Aeronautics and Space Administration

Langley Research Center Hampton, Virginia 23681-2199

The use of trademarks or names of manufacturers constitute an official endorsement, either expressed National Aeronautics and Space Administration.	in the report is for accurate reporting and does not or implied, of such products or manufacturers by the
Available from:	
NASA Center for AeroSpace Information (CASI) 7121 Standard Drive Hanover, MD 21076-1320 (301) 621-0390	National Technical Information Service (NTIS) 5285 Port Royal Road Springfield, VA 22161-2171 (703) 605-6000

MEMBRANE VIBRATION TESTS USING SURFACE-BONDED PIEZOELECTRIC PATCH ACTUATION

James L. Gaspar

Research Engineer Structural Dynamics Branch NASA Langley Research Center Hampton, VA 23681

Richard S. Pappa

Senior Research Engineer Structural Dynamics Branch NASA Langley Research Center Hampton, VA 23681

ABSTRACT

This paper describes the status of on-going work at the NASA Langley Research Center to measure the dynamics of thin membranes. The test article is a one-meter square pre-tensioned Kapton membrane that incorporates small surface-bonded piezoelectric patches strategically positioned to excite many modes. It is shown that PVDF (polyvinylidene fluoride) and MFC (macro fiber composite) piezoelectric patch actuators provide adequate excitation energy to obtain modal frequencies and mode shapes. Results from modal tests performed on the membrane using piezoelectric patches of different sizes and positions are discussed.

1. INTRODUCTION

With the increasing interest in large ultra-lightweight space structures and the desire for further exploration and discovery in space, revolutionary concepts for large antennas and observatories, solar sails, inflatable solar arrays and concentrators, are being studied by NASA^[1-3]. These systems will use new, ultra-lightweight materials. In the next few years, prototype hardware will be produced and will require structural testing and validation. Researchers have demonstrated that thin piezoelectric actuators can be used for modal testing ultra-lightweight inflation stiffened torus structures[4-6]. However, to the author's knowledge, no one has yet investigated using piezoelectric actuators for modal testing pre-tensioned flat membranes. Also, only a few experimental studies concerning the vibration of pre-tensioned flat membranes

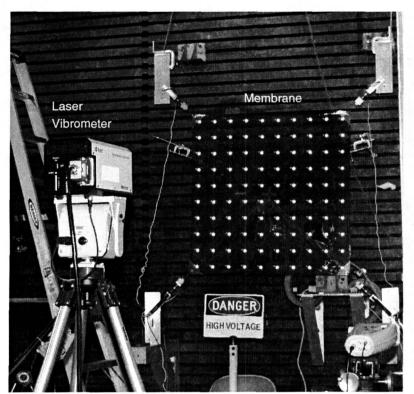
for space structures applications have been performed^[7-12]. These tests focused on using an electrodynamic shaker or impact hammer for modal excitation. Future space structures will have large sections of pre-tensioned flat membranes that will need to be vibration tested and validated. Their delicate nature requires the use of novel excitation methods and non-contacting structural measurement techniques. Laser vibrometry for vibration measurement with surface-bonded piezoelectric patches for excitation is one candidate technology for this purpose.

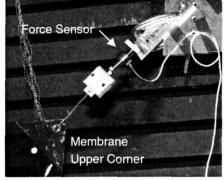
The research reported in this paper was conducted to begin to address the technical challenges and requirements of modal testing for future ultra-lightweight and inflatable space structures. Specific objectives of this work are to investigate the effectiveness (i.e., accuracy, precision, repeatability, etc.) of laser vibrometer measurements obtained on a thin pre-tensioned flat membrane actuated with surface-bonded piezoelectric patches of various sizes and positions on the membrane.

2. TEST ARTICLE AND EXPERIMENTAL PROCEDURE

2.1 Description of Test Article

The test specimen is a 1.02 m (40 in) square polyimide Kapton membrane with a thickness of 51 micron (2 mil). Figure 1 shows the test configuration for this study. Each of the corners of the material are reinforced using 128 micron (5 mil) thick transparency film on both sides. All four corners of the article are attached with 76.1 mm (3 in) wire through 6 mm diameter brass grommets. Linear





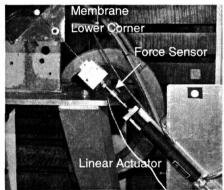


Figure 1: Experimental Test setup

actuators at the two lower corner locations are used to precisely preload the membrane. Force gauges are used to determine tension at each of the four corners. The tensioning devices are supported by aluminum brackets mounted to a heavy steel wall.

2.2 Actuator Description

The test article is excited using ceramic and polymer based piezoelectric patches. The ceramic based patches were developed at NASA Langley and are referred to as MFC's (Macro Fiber Composites)[13-14]. The polymer based piezoelectric patches are made with PVDF (Polyvinylidene Flouride) of various sizes manufactured by Measurement Specialties Inc. (MSI). The PVDF actuators consist of an active area covered with silver ink electrodes on both surfaces. The silver ink can withstand the high voltages required to drive the actuators. actuators also have an unmetallized border to eliminate the potential for arcing across the film thickness. The PVDF patches are much thinner than the MFC patches, and have a better impedance match with the Kapton membrane test article. However, the PVDF's have significantly less strain actuation capabilities than the MFC's. Patches of different sizes and positions on the membrane were used to determine their capability for

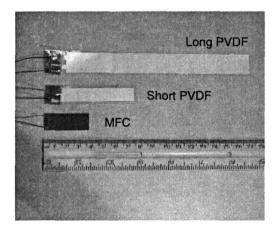


Figure 2: Piezoelectric Patches

exciting the membrane modes. Figure 2 shows the piezoelectric patches used. The long and short PVDF's are 52 microns thick, while the bottom actuator shown in the figure is the MFC with a thickness of 479 microns.

2.3 Surface-Bonding and Wiring Method

The piezoelectric patches are surface-bonded to the backside of the membrane with 3M 501FL double-backed adhesive transfer tape with an adhesive layer thickness of 51 microns. The MFC patches could easily be removed

and reused for other tests. Some of the PVDF patches had a tendency to tear when removed from the membrane and could not be reused. For the PVDF actuators, thin strain gage wire is attached to the actuator leads with 3M Z-Axis conductive tape. Kapton tape encapsulated the PVDF wire-leads for improved bond strength. The strain gage wires are soldered to the MFC leads. For all tests performed, the actuator wires were carefully secured to minimize their effect on the membrane vibrations.

2.4 Actuator Locations

Surface-bonded piezoelectric patches apply a strain to the membrane test article when voltage is applied. piezoelectric material will expand and contract in-phase with the input voltage signal. Thus, the surface-bonded actuators provide a small out-of-plane disturbance on the membrane due to the bending caused by the shear force created at the interface of the patch to the membrane. This bending can be seen as a small bulge on the surface of the membrane at the actuator location. The out-ofplane disturbance is capable of exciting the vibration modes of the structure when the actuator is strategically positioned on the membrane. Piezoelectric patches are most effective at strain anti-nodes, where the strain is high in the direction of the actuator. This is different from a traditional shaker modal test, where the shaker is most effective at displacement anti-nodes. Many actuator locations were tested to determine how to excite various modes of the membrane. The various actuator patch locations, shown in Figure 3, included excitation near the corners as well as within the body of the membrane.

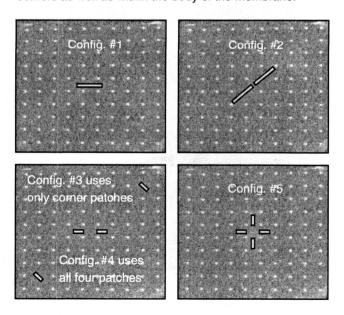


Figure 3: Actuator Configurations

2.5 Vibration Measurement Method

A Polytec PSV-300-H scanning laser vibrometer system is used to measure vibration of the test article. To provide more accurate measurements, 100 retro-reflective dots are adhered to the membrane in a grid pattern at even spacing of 101.6 mm (4 in) to allow for increased reflection of the laser beam to the laser vibrometer. The Polytec software is used to view frequency response functions (FRF's) and operating deflection mode shapes.

2.6 Test Description

All tests are performed with the membrane at a 20 N (4.6) lbf) tension level. Also, all tests apply a periodic chirp input signal with a bandwidth of 0 to 30 Hz to the The periodic chirp signal from the signal actuators. generator is used as the reference for the FRF calculations. To actuate the piezoelectric patches, the signal is amplified by 200 volts-per-volt with a Trek amplifier (Model PZD700) to produce a maximum input voltage of 1400 volts peak-to-peak (±700 volts). The FRF's are computed using 10 ensemble averages and a 256 Hz sample rate. The duration of each test is approximately 80 minutes to acquire all 100 FRF's. All of the vibration measurements in this report were made at ambient temperature and pressure conditions inside the high bay of the Structural Dynamics Laboratory located at the NASA Langley Research Center.

3. DISCUSSION OF TEST RESULTS

As with any modal test, accurate positioning of the actuators was found to be crucial for obtaining high quality modal data. A pretest finite element model was used to help evaluate high strain areas at each resonance, and modal test results were reviewed to locate the mode shape anti-nodes to determine good actuator locations. Few tests were able to excite all of the first five dominant modes well. The results from testing the membrane with various actuator configurations are discussed below.

3.1 One Long PVDF at Center Location

Figure 4 shows the coherence and mode shapes for the first five dominant modes excited using a single large PVDF actuator positioned at the center of the membrane. The coherence measurement indicates the degree of correlation between the input signal and the response signals. The coherence is used to assess the quality of the mode shapes obtained at resonance, with values

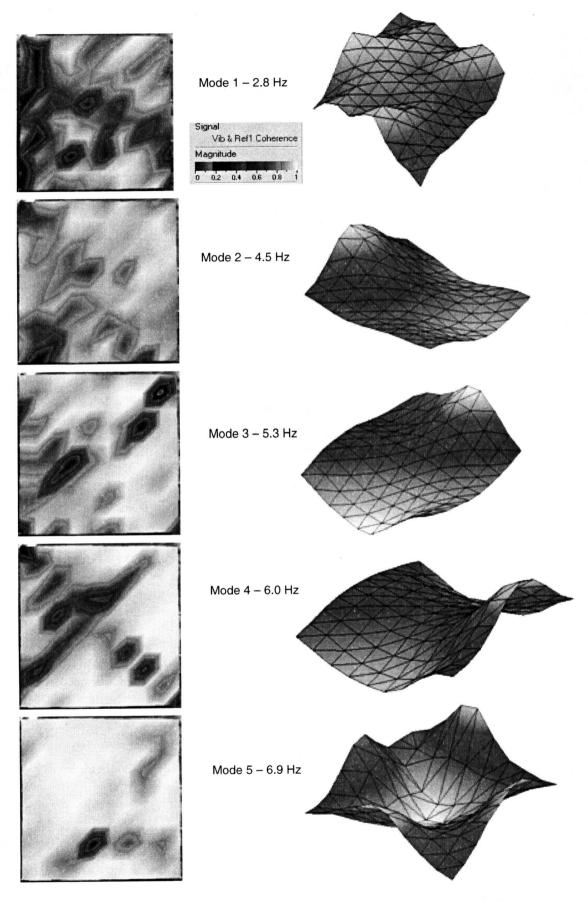


Figure 4: Coherence and Mode Shapes Obtained from Actuator Configuration #1

above 0.9 (light shade) over a large portion of the membrane surface considered to be good. The coherence plot, on the left side of Figure 4, shows how the coherence value changes across the surface of the membrane with the lightest shade being a high value above 0.9 and the darker shades decreasing in approximately 0.2 increments. These coherence plots show that four of the five modes are excited well with high coherence values and smooth symmetric mode shapes. The few low coherence values occur near node lines (locations with low motion), where the signal-to-noise ratio is poor and low coherence is acceptable.

The first mode at 2.8 Hz is poorly excited, as can be seen by the low coherence values along the left edge and over large portions within the body of the membrane. As a result, the mode shape for this mode is erratic and unsymmetric. This mode was rather difficult to excite for the majority of the tests performed on the membrane, regardless of excitation location. One reason for this is due to the fact that the mode is easily excited by ambient air effects in the lab, as shown by the frequency response in Figure 5. The figure shows the actuator did not excite the first mode much better than that obtained by ambient noise.

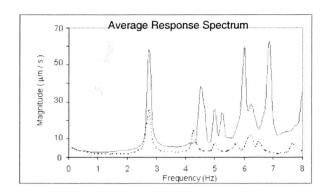


Figure 5: Config. #1 (Solid) vs. Ambient Noise (Dashed)

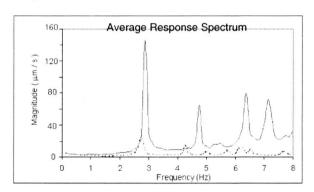


Figure 6: Config. #2 (Solid) vs. Ambient Noise (Dashed)

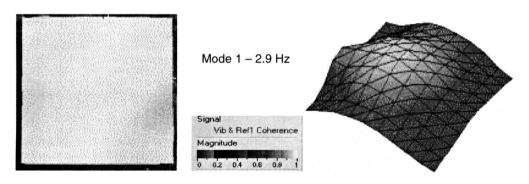


Figure 7: Coherence and Mode Shape Obtained from Actuator Configuration #2

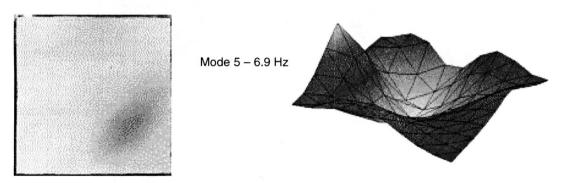


Figure 8: Coherence and Mode Shape Obtained from Actuator Configuration #3

3.2 Two Long PVDF's along Diagonal

Improved excitation of the first mode is obtained by using two long PVDF actuators located along a diagonal of the membrane at its center, as illustrated in Figure 3 (Configuration #2). Figures 6 and 7 show a significant improvement in frequency response, coherence, and mode shape.

3.3 Two Small MFC's at Opposite Corner Locations

Some attempts were made at exciting various modes with multiple actuators activated in-phase using the same input voltage periodic chirp signal. Configuration #3 (see Figure 3) excited mode 5 well by driving two small MFC actuators at opposite corners of the membrane. The mode shape and coherence is shown in Figure 8.

3.4 Four Small MFC's (2 at Center, 2 at Corners)

Two MFC actuators were added to the center and excited in-phase with the two corner actuators discussed for configuration #3, in an attempt to excite the other dominant modes (see configuration #4, Figure 3). However, the center actuators just distorted the mode shape for mode 5. Better control over which actuators are active at various frequencies may produce improved results.

3.5 Four Short Patches at Center (MFC versus PVDF)

Actuator configuration #5, shown in Figure 3, is used to evaluate the performance of the short PVDF and MFC patches. The MFC configuration did not excite mode 4 as well as the other modes. This may be due to the fact that this mode does not have a mode shape that is symmetric about the center of the membrane. Since the actuators are driven in-phase, they have a tendency to excite the mode shapes that are symmetric about the center of the membrane. Modes 2 and 3 are not symmetric about the center either, but they have a node line along one axis. Similar results are obtained with the short PVDF actuators, which is significant because they have much lower strain capability than the MFC's and a closer impedance match with the membrane.

4. CONCLUSIONS

Surface-bonded piezoelectric patches of different sizes were used to perform modal tests on a thin pre-tensioned membrane using various excitation locations. It was

shown that surface-bonded piezoelectric patches provide adequate excitation energy to obtain modal frequencies and mode shapes on thin pre-tensioned flat membranes. However, good mode shapes were difficult to obtain and highly dependant on selecting a suitable location to properly excite the desired modes. It is believed that further work investigating optimum multi-point excitation locations and selectively controlling the energy input to each individual actuator over various frequency bandwidths will provide better results.

5. ACKNOWLEDGEMENTS

The authors would like to thank Dr. Keats Wilkie of NASA Langley for helpful discussions and for providing the MFC's.

REFERENCES

- [1] "The Gossamer Spacecraft Initiative: Technology to See the Unseen Universe," First Gossamer Workshop, Oxnard, CA, October 1999.
- [2] Chmielewski, A. B., Moore, C., and Howard, R., "The Gossamer Initiative," IEEE paper 0-7803-5846-5/00, January 2000.
- [3] First Gossamer Spacecraft Forum, Held in Conjunction With the AIAA Structures, Structural Dynamics, and Materials Conference, Atlanta, GA, April 2000.
- [4] Agnes, G. S., Rogers, J. W., "Piezoelectric Excitation of Inflatable Space Structures for Modal Testing," Proc. 7th SPIE Int. Symp. On Smart Structures and Materials, Newport Beach, CA, March 5-9, 2000.
- [5] Park, G., Kim, M., Mandin, M., and Inman, D. J., "Vibration Control of Inflatable Space Structures using Smart Materials," Proc. 18th ASME Biennial Conf. on Mechanical Vibration and Noise, Pittsburgh, PA, September 9-12, 2001.
- [6] Park, G., Ruggiero, E., Inman, D. J., "Dynamic Testing of Inflatable Structures using Smart Materials," Smart Materials and Structures Volume 11, Number 1, February 2002.
- [7] Sewall, J. L., Miserentino, R., and Pappa, R. S., "Vibration Studies of a Lightweight Three-Sided Membrane Suitable for Space Application," NASA TP-

- 2095, January 1983.
- [8] Singhal R. K., Gorman D. J., Crawford J.M., and Graham W. B. (1994), "Investigation of the Free Vibration of a Rectangular Membrane," AIAA Journal 32, pp. 2456-2461.
- [9] Kukathasan, S., "Vibration of Prestressed Membrane Structures," Master's Thesis, University of Cambridge, Department of Engineering, August 2000.
- [10] Johnston, J. and Lienard, S., "Modeling and Analysis of Structural Dynamics for a One-Tenth Scale Model NGST Sunshield," Proceedings of the 42nd AIAA/ASME/ASCE/AHS/ACS Structures, Structural Dynamics, and Materials Conference, Seattle, WA, April 16-19, 2001, AIAA-2001-1407.
- [11] Flint, E. M., Glaese, R. M., "Characterization, Prediction, and Improvement of Stretched Flat Hexagonal Gossamer Membrane Dynamic Response," Proc., 42nd AIAA/ASME/ASCE/AHS/ACS Structures, Structural Dynamics, and Materials Conference, Seattle, WA, April 16-19, 2001, AIAA-2001-1410.
- [12] Gaspar, J. L., Solter, M. J., Pappa, R. S., "Membrane Vibration Studies Using a Scanning Laser Vibrometer," Proc. of the 20th International Modal Analysis Conference, Los Angeles, CA, 2002.
- [13] Wilkie, W. K., Bryant, G. R., High, J. W. et al., "Low-Cost Piezocomposite Actuator for Structural Control Applications," Proceedings, SPIE 7th Annual International Symposium on Smart Structures and Materials, Newport Beach, CA, March 5-9, 2000.
- [14] Williams, R. B., Park, G., Inman, D. J., Wilkie, W. K., "An Overview of Composite Actuators with Piezoceramic Fibers," Proc. of the 20th International Modal Analysis Conference, Los Angeles, CA, 2002.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for re sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send commaspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budg			reviewing instructions, searching existing data
aspect of this collection of information, incl Reports, 1215 Jefferson Davis Highway,	uding suggestions for reducing this burden, t Suite 1204, Arlington, VA 22202-4302, and to	o Washington Headquarters Service the Office of Management and Bu	es, Directorate for Information Operations and idget, Paperwork Reduction Project (0704-0188),
Washington, DC 20503. 1. AGENCY USE ONLY (Leave bland)			PE AND DATES COVERED
I. Adendi dde dieli (Edave Bian	February 2003		Memorandum
4. TITLE AND SUBTITLE			5. FUNDING NUMBERS
Membrane Vibration Tes	sts Using Surface-Bonded Piez	oelectric Patch	
Actuation			WU- 755-06-00-21
6. AUTHOR(S)			
James L. Gaspar and Ric	hard S. Pappa		
7. PERFORMING ORGANIZATION	NAME(S) AND ADDRESS(ES)		8. PERFORMING ORGANIZATION
, , , , , , , , , , , , , , , , , , ,	(0, , , , ,)		REPORT NUMBER
NASA Langley Research	Center		
Hampton, VA 23681-219	99		L-18261
9. SPONSORING/MONITORING AG	SENCY NAME(S) AND ADDRESS(ES)		10. SPONSORING/MONITORING AGENCY REPORT NUMBER
National Aeronautics and	Space Administration		
Washington, DC 20546-0			NASA/TM-2003-212150
11. SUPPLEMENTARY NOTES	·		
Presented at the 21 st Inter	national Modal Analysis Conf	ference (IMAC); Kissim	nmee, Florida; February 3-6, 2003.
12a. DISTRIBUTION/AVAILABILITY	STATEMENT		12b. DISTRIBUTION CODE
Unclassified-Unlimited			1.23. 5.5. 11.1.50 11.6.11 0052
Subject Category 39	Distribution: Standard		
Availability: NASA CAS			
13. ABSTRACT (Maximum 200 word	ts)	<u> </u>	
	status of on-going work at the		
=	nnes. The test article is a one-i		-
	e-bonded piezoelectric patches inylidene fluoride) and MFC (
	on energy to obtain modal free	•	•
	ane using piezoelectric patches	-	
performed on the memore	ane using prezenteure patener	of different sizes and p	ositions are discussed.
14. SUBJECT TERMS			15 MIMPER OF PACES
	nning laser vibrometer; Gossa	mer spacecraft dynamic	15. NUMBER OF PAGES
	ctural dynamics testing; Exper	•	16. PRICE CODE
17. SECURITY CLASSIFICATION	18. SECURITY CLASSIFICATION OF THIS PAGE	19. SECURITY CLASSIFIC	ATION 20. LIMITATION
OF REPORT Unclassified	Unclassified	OF ABSTRACT Unclassified	OF ABSTRACT UL
		Cholassinou	Ü.
NSN 7540-01-280-5500	·		Standard Form 298 (Rev. 2-89)

Standard Form 298 (Rev. 2-89) Prescribed by ANSI Std. Z-39-18 298-102

•			
I I			
i I			